## Demo on the interpretation of the $H_{\infty}$ norm of linear systems:

Let us consider a linear system G(s) with:

- n = 6 states,
- m = 2 inputs and
- p = 3 outputs:

```
warning('off');
G=ss([-0.5 5 0 0 0;-5 -0.5 0 0 0;0 0 -8 0 0;...
0 0 0 -8 0 0;0 0 0 0 -4.5 1.5; 0 0 0 0 -1.5 -4.5],...
[0.5 -0.9;0.5 0.4;1.2 0.13;1.5 -2.33; -0.5 -0.3;2.2 1.8],...
[-0.7 1.3 0.2 1.1 0.75 0.2;-0.4 -1.1 -1 -2.3 0.2 0.5;...
-0.4 -0.5 0 0.9 0.4 0.5],[-0.9 0;1.2 -3.1;1.6 0.6]);
size(G)
```

State-space model with 3 outputs, 2 inputs, and 6 states.

```
By definition \|\mathbf{G}(s)\|_{\infty} = \max \sigma_{\max}(\mathbf{G}(j\omega))
```

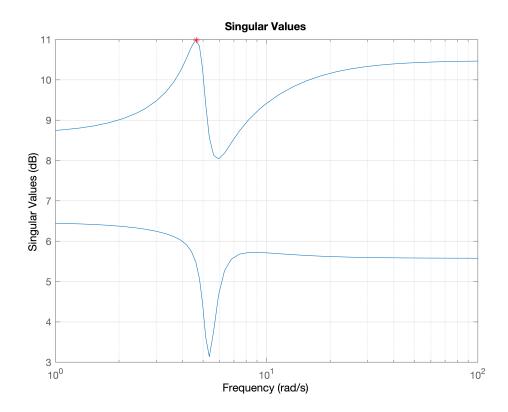
norm(G, 'inf')

```
ans = 3.5431
```

 $\|\mathbf{G}(s)\|_{\infty}$  is the peak of the frequency-domain response of the singular values of  $\mathbf{G}(j\omega)$ . The frequency  $\omega_{wc}(rad/s)$  of the peak can be found thanks to the function hinfnorm:

```
[gain,w_wc]=hinfnorm(G)
gain = 3.5431
w_wc = 4.6517
figure
sigma(G);
grid
hold on
```

plot(w wc,20\*log10(gain),'r\*')



The property:  $\|\mathbf{G}(s)\|_{\infty} = \sup_{U(s)\in H_2} \frac{\|\mathbf{Y}(s)\|_2}{\|\mathbf{U}(s)\|_2}$  can be interpreted considering the steady state harmonic response of the system at the frequency  $\omega_{wc}$ . Indeed the Singular Value Decomposition (SVD) of  $\mathbf{G}(j\omega_{wc})$  reads:

$$\mathbf{G}(j\omega_{wc}) = \begin{bmatrix} \mathbf{u}_1 & \mathbf{u}_2 & \mathbf{u}_3 \end{bmatrix} \begin{bmatrix} \sigma_{\max}(\omega_{wc}) & 0\\ 0 & \sigma_{\min}(\omega_{wc})\\ 0 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{v}_1^*\\ \mathbf{v}_2^* \end{bmatrix} \,.$$

( $x^*$  is the transconjugated of x.). All  $\mathbf{u}_i$  ( $i = 1, \dots, p$ ) and  $\mathbf{v}_i$  ( $j = 1, \dots, m$ ) are unitarty vectors. Thus:

$$\sigma_{\max}(\omega_{wc}) = \|\mathbf{G}(s)\|_{\infty} = \mathbf{u}_1^* \mathbf{G}(j\omega_{wc}) \mathbf{v}_1.$$

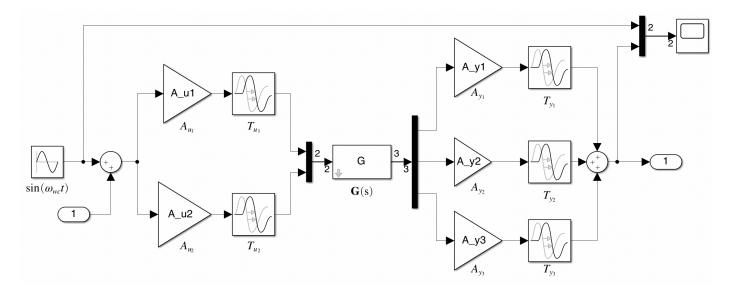
The complex components of  $\mathbf{v}_1$  (resp.  $\mathbf{u}_1^*$ ) gives the combination of the harmonic inputs (resp. outputs) leading to the worst (or the highest) magnitude at the frequency  $\omega_{wc}$ .

Each component of  $\mathbf{u}_1^*$  or  $\mathbf{v}_1$  can be expressed under the form  $Ae^{j\phi}$  where *A* is the magnitude and  $\phi$  is the phase or under the form  $Ae^{-jT\omega_{wc}}$  where *T* is a delay providing the phase lag  $\phi$  at the frequency  $\omega_{wc}$ .:

• 
$$T = -\phi/\omega_{wc}$$
, if  $\phi \in [0, -\pi]$ 

•  $T = -(\phi - 2\pi)/\omega_{wc}$ , if  $\phi \in [0, \pi]$ .

Thus, from the  $3 \times 2$  MIMO system  $\mathbf{G}(s)$ , it is possible to build a SISO real system whose the highest magnitude frequency response is at  $\omega_{wc}$  with a magnitude of  $\|\mathbf{G}(s)\|_{\infty}$ . This system is described by the following block-diagram



with:

$$\mathbf{v}_{1} = \begin{bmatrix} -jT_{u_{1}}\omega_{wc} \\ A_{u_{1}}e^{-jT_{u_{2}}\omega_{wc}} \\ A_{u_{2}}e^{-jT_{u_{2}}\omega_{wc}} \end{bmatrix} \text{ and } \mathbf{u}_{1}^{*} = \begin{bmatrix} A_{y_{1}}e^{-jT_{y_{1}}\omega_{wc}} & -jT_{y_{2}}\omega_{wc} \\ A_{y_{2}}e^{-jT_{y_{2}}\omega_{wc}} & A_{y_{3}}e^{-jT_{y_{3}}\omega_{wc}} \end{bmatrix}.$$

The following sequence illustrated the frequency-response at  $\omega_{wc}$ .

```
G_M=freqresp(G,w_wc);
[U,S,V]=svd(G_M);
U(:,1)'*G_M*V(:,1)
```

ans = 3.5431 - 0.0000i

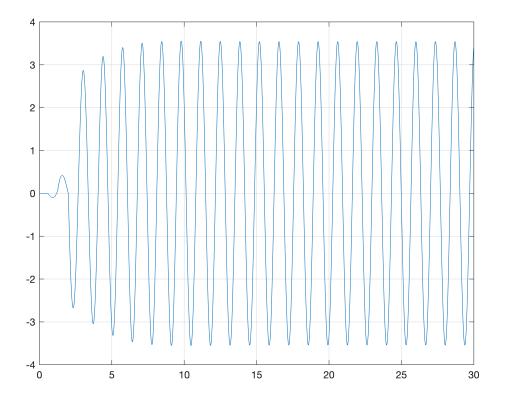
This results illustrates that:  $\sigma_{\max}(\omega_{wc}) = \|\mathbf{G}(s)\|_{\infty} = \mathbf{u}_1^* \mathbf{G}(j\omega_{wc}) \mathbf{v}_1$ .

```
% Worst magnitude and phase distribution for harmonic inputs at w_wc:
% (with the constraint sum(A_ui^2)=1)
A_ul=abs(V(1,1));
phi_ul=angle(V(1,1));
if phi_ul>0,phi_ul=phi_ul-2*pi;end
A_u2=abs(V(2,1));
phi_u2=angle(V(2,1));
if phi_u2>0,phi_u2=phi_u2-2*pi;end
% phase equivalent delay at the frequency w_wc:
T_ul=-phi_ul/w_wc;
T_u2=-phi_u2/w_wc;
% Worst magnitude and phase combination of the outputs:
% (with the constraint sum(A_yi^2)=1)
```

```
A_y1=abs(U(1,1)');
phi_y1=angle(U(1,1)');
if phi_y1>0,phi_y1=phi_y1-2*pi;end
A_y2=abs(U(2,1)');
phi_y2=angle(U(2,1)');
if phi_y2>0,phi_y2=phi_y2-2*pi;end
A_y3=abs(U(3,1)');
phi_y3=angle(U(3,1)');
if phi_y3>0,phi_y3=phi_y3-2*pi;end
% phase equivalent delay at the frequency w_wc:
T_y1=-phi_y1/w_wc;
T_y2=-phi_y2/w_wc;
T_y3=-phi_y3/w_wc;
```

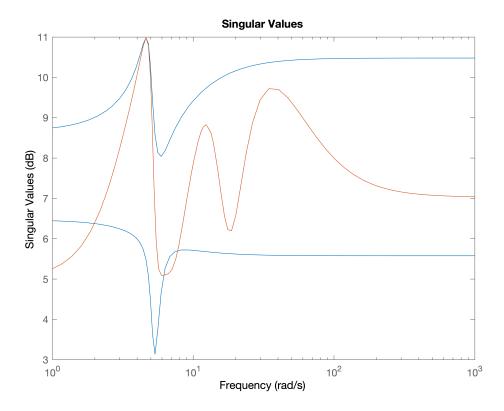
**Simulation:** the following SIMULINK system is a SISO real system with the same  $H_{\infty}$  norm than **G**(s) (up to the approximation of the delay).

```
simul_wc_harmonic
SimOut=sim('simul_wc_harmonic');
figure
plot(SimOut.yout{1}.Values.time,SimOut.yout{1}.Values.Data)
grid
```



The magnitude of the oscillations (in steady state) is equal to  $\|\mathbf{G}(s)\|_{\infty}$ .

```
[a,b,c,d]=linmod('simul_wc_harmonic');
figure
```



The SISO SIMULINK sygstem and G(s) have the same  $H_{\infty}$  norm.

Thus, for a MIMO system,  $\|\mathbf{G}(s)\|_{\infty}$  gives the magnitude in steady state of the response of the "worst" complex combination of the outputs to an harmonic signal at the critical frequency  $\omega_{wc}$  with the worst complex distribution on the inputs.